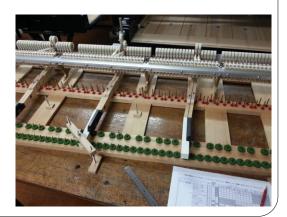
Grand Action Set Up



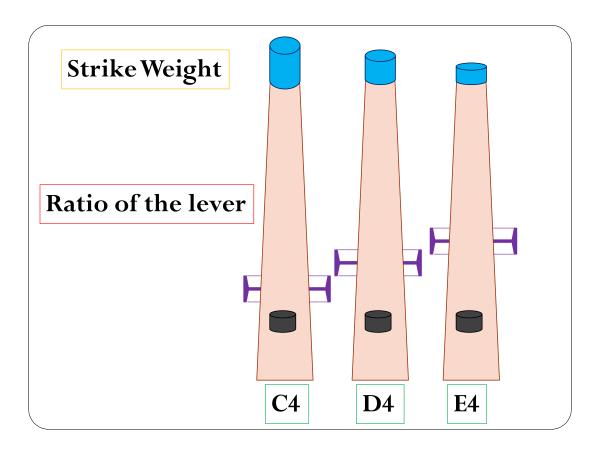
Contents of Class

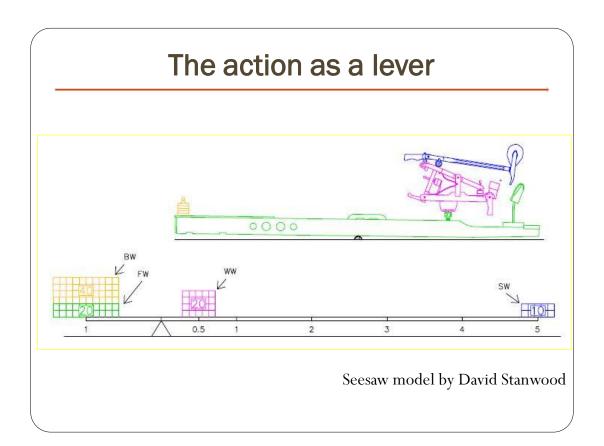
- ❖ Basic Measurement & Geometry
- Touchweight related ratios and weights
- Some sample procedures

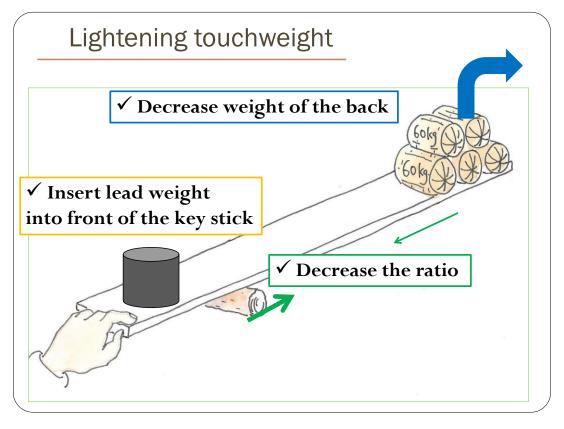


- **C4** is set up **heavier**
- **&** E4 is set up **lighter**

That relates Ratios & Weights







Basics, Ratios & Weights

- 1. Basic measurement
- 2. Action ratio, view from regulation
- 3. Strike ratio, view from static touchweight
- **4. Gear ratios** and linked Moment of Inertia, view from kinetic touchweight
- 5. Strike Weight, majority of the touchweight
- 6. Front Weight, locating key leads

1, Basic measurement

***** Spread Distance



❖ Magic line

Key – Whippen connection



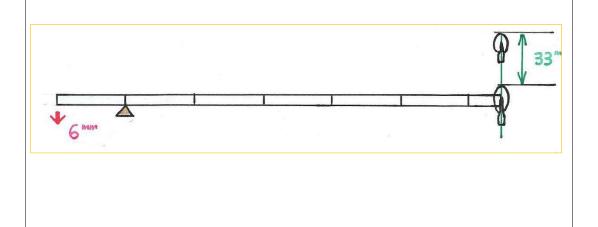
Check when capstan crosses connecting point

Center pin height



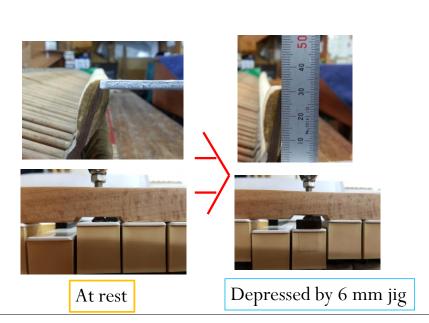
2, Action Ratio, view from travel distance

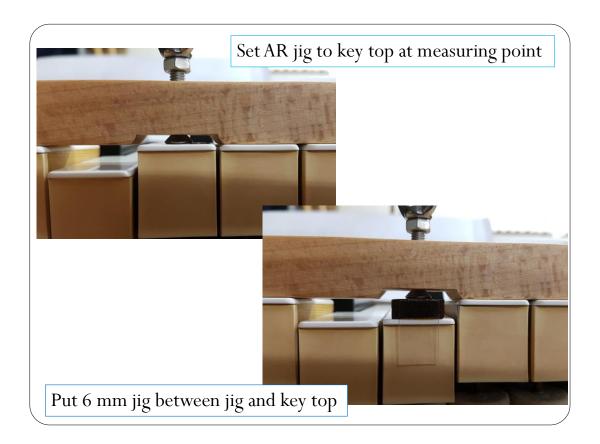
$$AR = 33 / 6 = 5.5$$



Measure how much hammer travels by 6 mm dip

Hammer travel distance / 6 = AR





Calculate key depth

Key dip = (hammer blow - let off) / AR + aftertouch

(Example) Key dip = (47 mm - 2 mm) / 5.5 + 1.5 mm= 45/5.5 + 1.5 = 9.7 mm

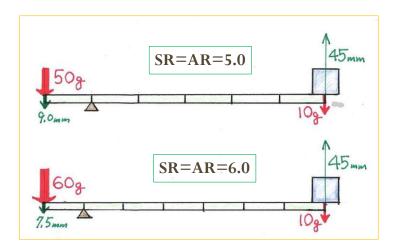
*at measuring point i.e. 13 mm from front edge



| Action Ratio | Key depth at front edge |
|--------------|-------------------------|
| 5.2 | 10.5 |
| 5.4 | 10.2 |
| 5.6 | 9.9 |
| 5.8 | 9.6 |
| 6.0 | 9.3 |
| 6.2 | 9.1 |

Figures at: hammer blow 46 mm, let off 2 mm, aftertouch 1.5 mm Key length (front side) 200 mm

3, Strike Ratio, view from Weight



Weight ratio between key front and hammer

The weight needed at key front when balanced 1 g of hammer

Take measurement

 $SR = ((FW + BW) - (WW \times KR)) / SW$









Calculate BW by measuring DW & UW

1, Measure DW & UW

2, Calculate : $\mathbf{BW} = (DW + UW) / 2$



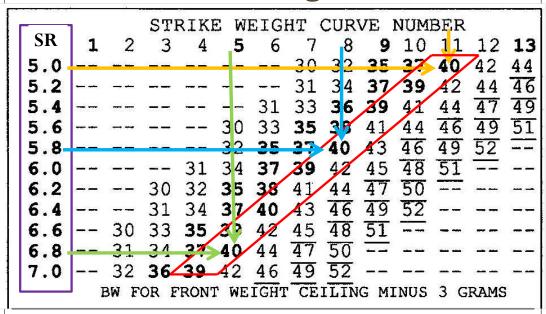
Measure SR by 2 g weight

SR = (BW with 2 g - BW without 2 g) / 2



Put 2 g weight inline with hammer center line

Workable range of SR

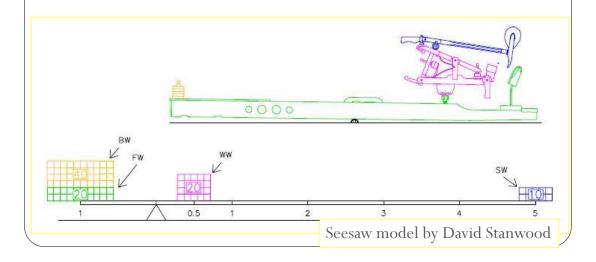


Parameter table by David Stanwood

4, Gear Ratio and Moment of Inertia

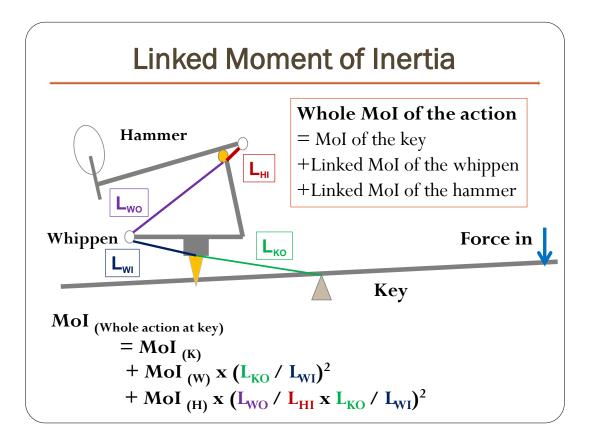
Torque = Moment of Inertia x Angular acceleration

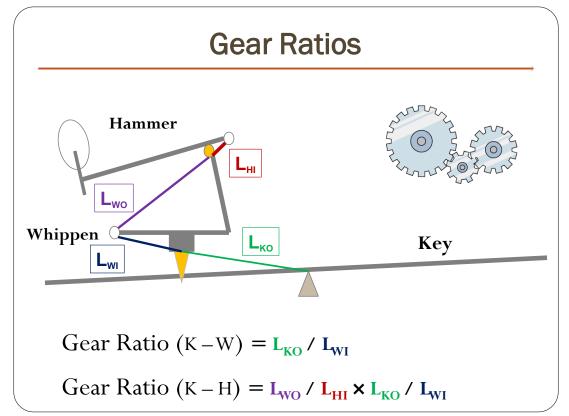
Strike force to the key = MoI x Angular Acceleration of the key



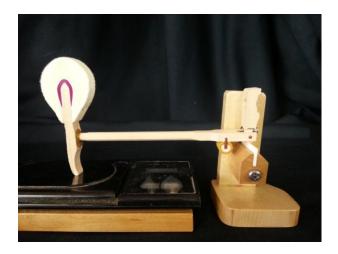
Each part has own Mol



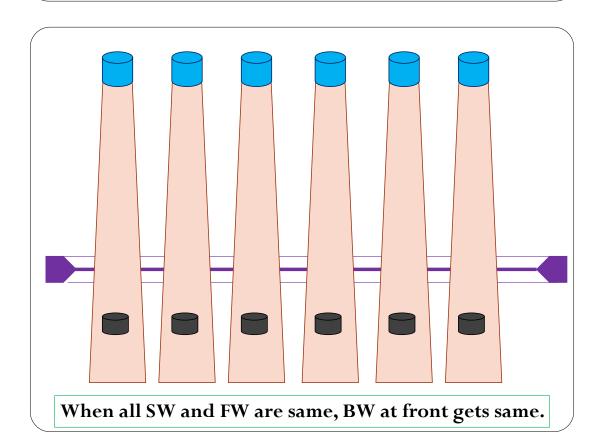


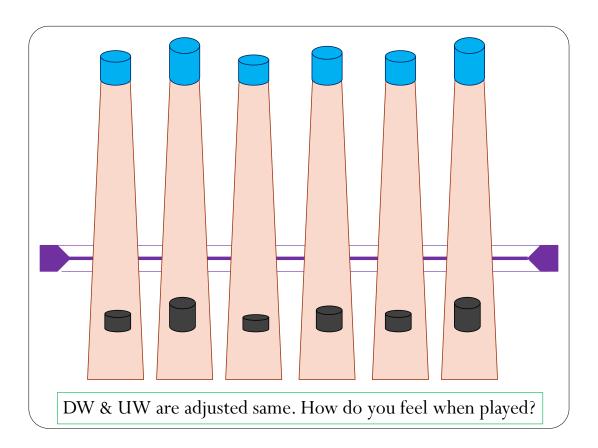


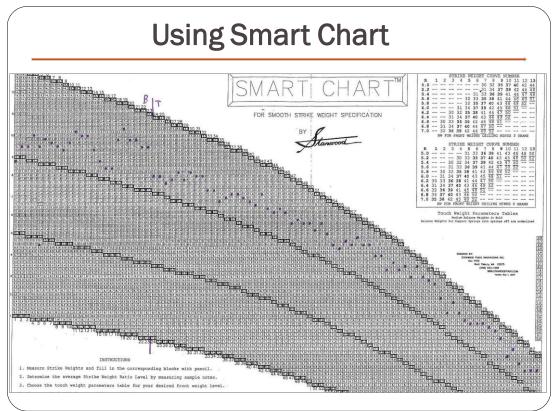
5, Strike Weight

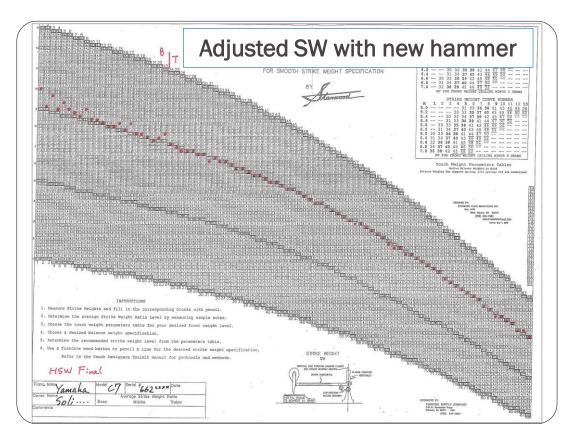


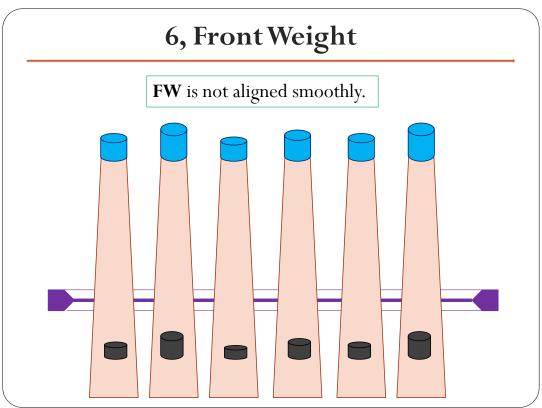
More than 80% of touchweight is coming from hammer

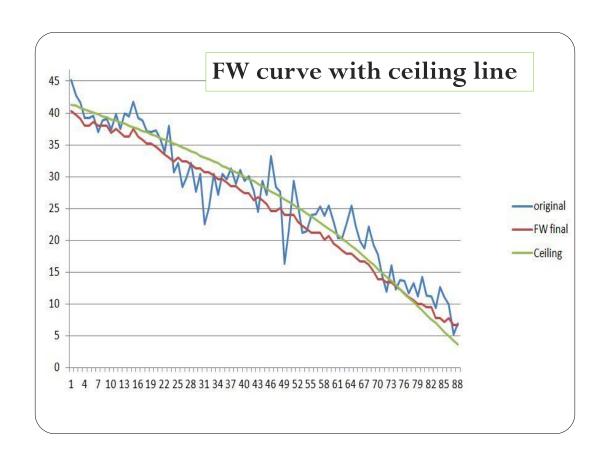




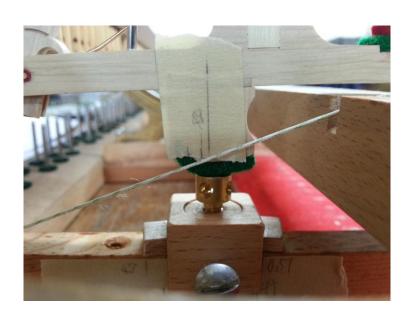








6, Set up the action, Procedure



Sample 1: only existing parts



S&S B # 50****

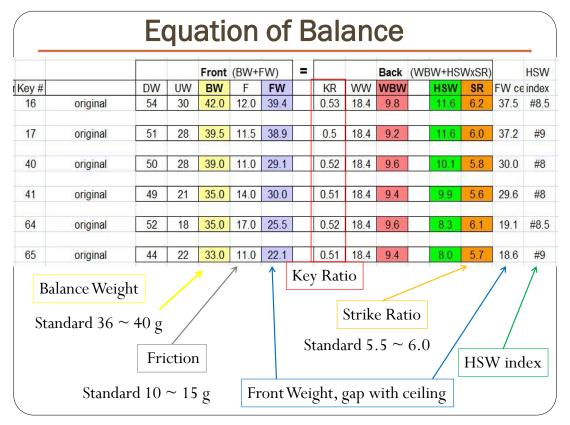
Someone put new hammers and shanks not so long ago.

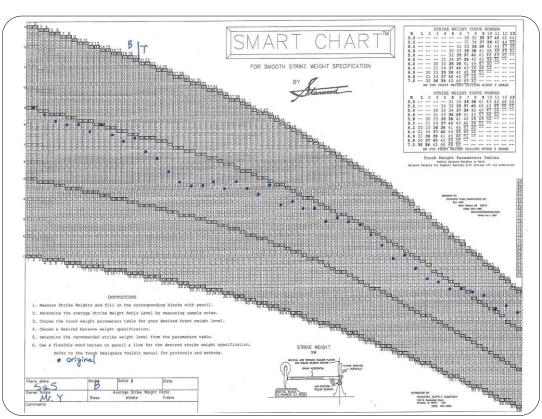
The customer wanted to;

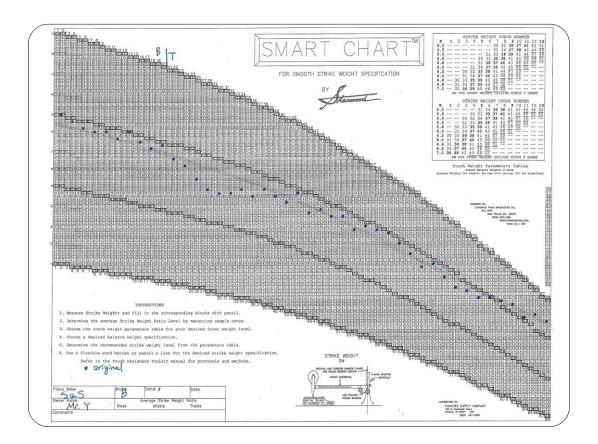
- make lighter slightly
- have smoother touch through all registers
- better response
- * It was difficult to play pp when playing lightly in tenor and bass area

Observation

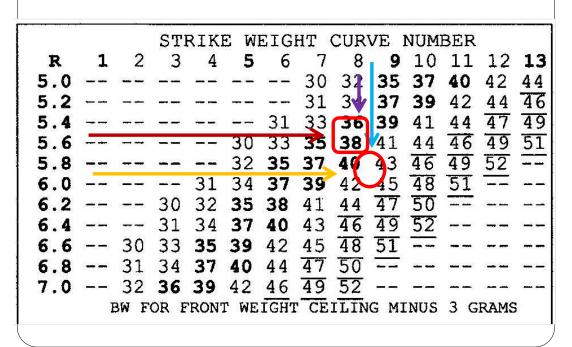
- ➤ Damper timing is too early
- ➤ Split wedge felts are too long in tenor section
- ➤ Action centers are tight
- The spread distance is shorter in tenor to bass
- ➤ Balance weight index is standard to a bit higher
- Key ratio is vary due to uneven positioning of capstans







Check parameter table



Simulate by equation of balance

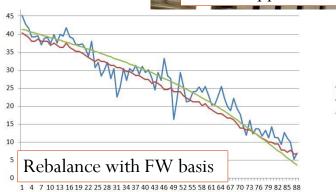
| Orig | inal + trial | | | Front | (BW+I | FW) | - | | | Back | (WBW+HS | WxSR) | | HSV |
|------|-------------------|----|----|-------|-------|------|----|------|------|------------|---------|-------|-------|------|
| Key# | | DW | UW | BW | F | FW | | KR | WW | WBW | HSW | SR | FW ce | inde |
| 16 | original | 54 | 30 | 42.0 | 12.0 | 39.4 | .0 | 0.53 | 18.4 | 9.8 | 11.6 | 6.2 | 37.5 | #8. |
| | shim whippen heel | 49 | 25 | 37.0 | 12.0 | 39.4 | | 0.53 | 18.4 | 9.8 | 11.6 | 5.7 | | |
| | re-balance | 52 | 28 | 40.0 | 12.0 | 36.4 | 8 | 0.53 | 18.4 | 9.8 | 11.6 | 5.7 | | |
| 17 | original | 51 | 28 | 39.5 | 11.5 | 38.9 | | 0.5 | 18.4 | 9.2 | 11.6 | 6.0 | 37.2 | #9 |
| | shim whippen heel | 46 | 23 | 34.5 | 11.5 | 38.9 | | 0.5 | 18.4 | 9.2 | 11.6 | 5.5 | | |
| | re-balance | 51 | 28 | 39.5 | 11.5 | 33.9 | 28 | 0.5 | 18.4 | 9.2 | 11.6 | 5.5 | | |

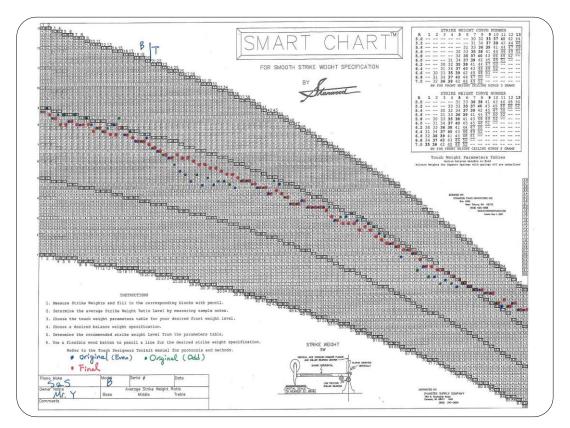
Actual work

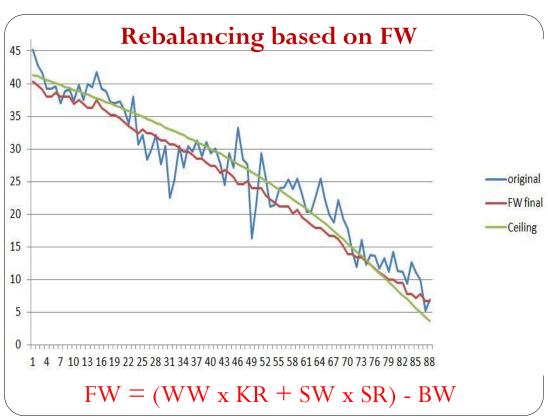
- ➤ Re-center flanges
- ➤ Correct spread distance
- ➤ Trim split wedge felts
- ➤ Adjust damper timing etc

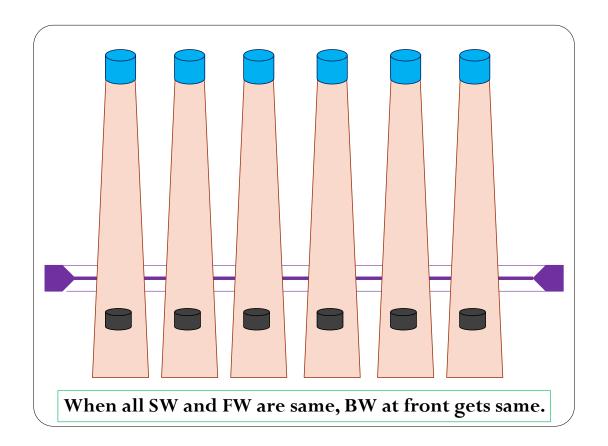






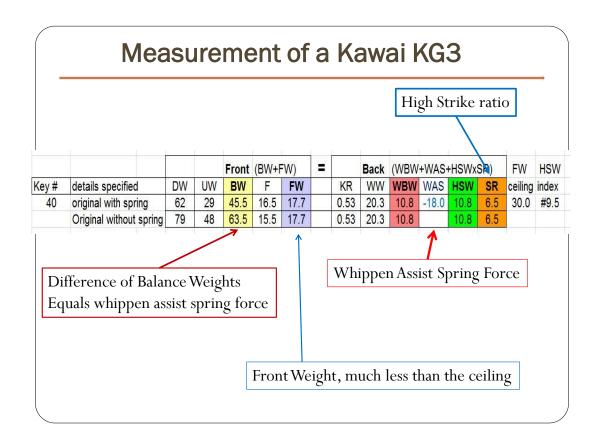




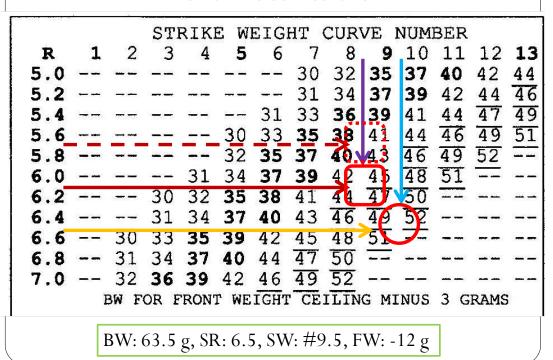


Sample 2: whippen assist spring





Parameter table



Plan 1

Rebalancing only

| | | | | Front | (BW+F | W) | = | | Back | (WBW | +WAS | +HSWx | SR) | FW | HSW |
|------|-------------------------|----|----|-------|-------|------|---|------|------|------------|-------|-------|-----|---------|-------|
| # | details specified | DW | UW | BW | F | FW | | KR | WW | WBW | WAS | HSW | SR | ceiling | index |
| an 1 | original with spring | 62 | 29 | 45.5 | 16.5 | 17.7 | | 0.53 | 20.3 | 10.8 | -18.0 | 10.8 | 6.5 | 30.0 | #9.5 |
| | Original without spring | 79 | 48 | 63.5 | 15.5 | 17.7 | | 0.53 | 20.3 | 10.8 | | 10.8 | 6.5 | | |
| | Key balancing | 55 | 24 | 39.5 | 15.5 | 41.7 | | 0.53 | 20.3 | 10.8 | | 10.8 | 6.5 | | |

FW gets more than 10 grams heavier than the ceiling

Plan 2

Reduce SW and SR then key balancing

| | | | | Front | (BW+F | W) | = | | Back | (WBW | +WAS- | +HSWx | SR) | FW | HSW |
|---|-------------------------|----|----|-------|-------|------|-----|------|------|------------|-------|-------|-----|---------|-------|
| | details specified | DW | UW | BW | F | FW | | KR | WW | WBW | WAS | HSW | SR | ceiling | index |
| 2 | original with spring | 62 | 29 | 45.5 | 16.5 | 17.7 | | 0.53 | 20.3 | 10.8 | -18.0 | 10.8 | 6.5 | 30.0 | #9.5 |
| | Original without spring | 79 | 48 | 63.5 | 15.5 | 17.7 | | 0.53 | 20.3 | 10.8 | | 10.8 | 6.5 | | |
| | SW adjustment | 76 | 45 | 60.5 | 15.5 | 17.7 | | 0.53 | 20.3 | 10.8 | 1 | 10.4 | 6.5 | | #8.5 |
| | Half cut punching | 72 | 41 | 56.5 | 15.5 | 17.7 | | 0.53 | 20.3 | 10.8 | | 10.4 | 6.1 | | |
| | Shim capstan | 68 | 37 | 52.5 | 15.5 | 17.7 | | 0.53 | 20.3 | 10.8 | | 10.4 | 5.7 | | |
| | Key balancing | 55 | 24 | 39.5 | 15.5 | 30.7 | | 0.53 | 20.3 | 10.8 | | 10.4 | 5.7 | | |
| | 1000 | 77 | | | | - | 111 | | | | | | | | |

FW is about the ceiling

Strike ratio gets standard

Plan 3

Reduce SW, SR and WAS then key balancing

| | | | | Front | (BW+F | FW) | = | | Back | (WBW | +WAS | +HSWx | SR) | FW | HSW |
|----|-------------------------|----|----|-------|-------|------|---|------|------|------|-------|-------|-----|---------|-------|
| # | details specified | DW | UW | BW | F | FW | | KR | WW | WBW | WAS | HSW | SR | ceiling | index |
| 13 | original with spring | 62 | 29 | 45.5 | 16.5 | 17.7 | | 0.53 | 20.3 | 10.8 | -18.0 | 10.8 | 6.5 | 30.0 | #9.5 |
| | Original without spring | 79 | 48 | 63.5 | 15.5 | 17.7 | | 0.53 | 20.3 | 10.8 | 8 | 10.8 | 6.5 | | |
| | SW adjustment | 76 | 45 | 60.5 | 15.5 | 17.7 | | 0.53 | 20.3 | 10.8 | | 10.4 | 6.5 | | #8.5 |
| | Half cut punching | 72 | 41 | 56.5 | 15.5 | 17.7 | | 0.53 | 20.3 | 10.8 | | 10.4 | 6.1 | | |
| | Weaken asist spring | 64 | 33 | 48.5 | 15.5 | 17.7 | | 0.53 | 20.3 | 10.8 | -8.0 | 10.4 | 6.1 | | |
| | Key balancing | 55 | 24 | 39.5 | 15.5 | 26.7 | | 0.53 | 20.3 | 10.8 | -8.0 | 10.4 | 6.1 | l l | |

Reduced whippen Assist spring force

Front Weight, 3 grams minus the ceiling

Sample 3: with new parts



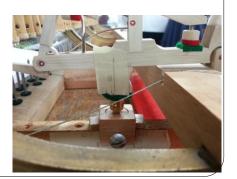
Change parameters

- ***** Friction
- **Geometry**
- **\$** SW, SR, WW, KR and BW
- **❖** Moment of Inertia and Gear ratio



Find desired geometry

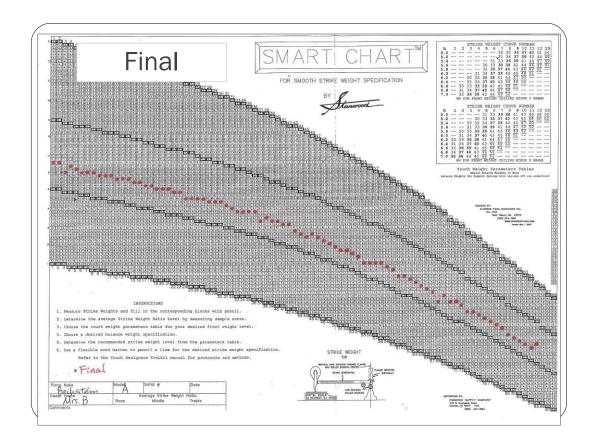
- ❖ Install new shank and a hammer which has similar SW of new hammer (or actual one)
- ❖ Install whippen with temporary fixed heel
- ❖Set temporary capstan to original position
- ❖ Check regulation with AR



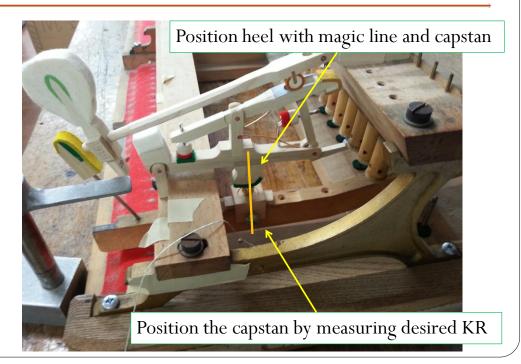
Adjust SW of new set of hammers

- 1. Weight raw hammer heads
- 2. Calculate SW or measure it with dummy shank
- 3. Pre-taper heavier ones
- 4. Measure SW after gluing shanks and chopped excess
- 5. Tail and taper hammer to get desired SW
- 6. Bore and add hammer lead if necessary

Purple: SW with dummy shall be a second of the first second of the secon



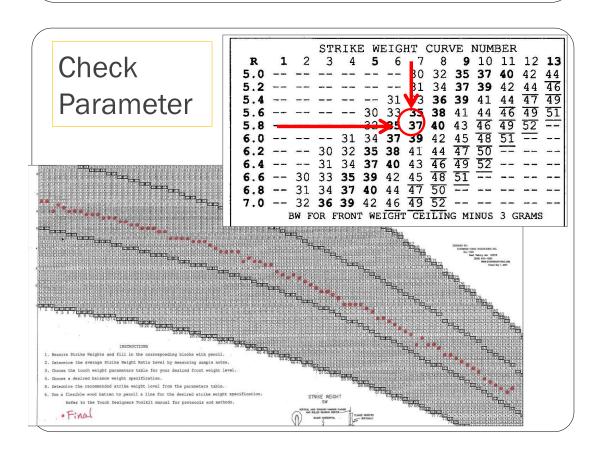
Position capstan and whippen heel



Check equation of balance

| | | | | Front | (BW+I | FW) | = | | | Back | (WBW | +HSW | xSR) | | HSW |
|-----|---|----|----|-------|-------|------|---|------|------|-------|------|------|------|-------|-------|
| Key | # details specified | DW | UW | BW | F | FW | | KR | WW | WBW | | HSW | SR | FW ce | index |
| 16 | original | 63 | 21 | 42.0 | 21.0 | 29.8 | | 0.54 | 19.3 | 10.4 | | 10.2 | 6.0 | 37.5 | #6 |
| | new hammer, shank & whippen, cut punching | 65 | 33 | 49.0 | 16.0 | 20.2 | | 0.52 | 16.6 | 8.6 | | 10.5 | 5.8 | | #6.5 |
| | rebalance | 56 | 24 | 40.0 | 16.0 | 29.2 | | 0.52 | 16.6 | 8.6 | | 10.5 | 5.8 | | |
| 17 | original | 56 | 13 | 34.5 | 21.5 | 36.0 | | 0.52 | 19.3 | 10.0 | | 9.7 | 6.2 | 37.2 | #5 |
| | new hammer, shank & whippen, cut punching | 57 | 27 | 42.0 | 15.0 | 26.5 | | 0.52 | 16.6 | 8.6 | | 10.4 | 5.8 | | #6.5 |
| | rebalance | 55 | 25 | 40.0 | 15.0 | 28.5 | | 0.52 | 16.6 | 8.6 | | 10.4 | 5.8 | | |
| 40 | original | 72 | 22 | 47.0 | 25.0 | 23.2 | | 0.53 | 19.2 | 10.18 | | 9.0 | 6.67 | 30 | #6 |
| | new hammer, shank & whippen, cut punching | 61 | 33 | 47.0 | 14.0 | 13.5 | | 0.52 | 16.6 | 8.63 | | 9.3 | 5.58 | | #6.5 |
| | rebalance | 54 | 26 | 40.0 | 14.0 | 20.5 | | 0.52 | 16.6 | 8.63 | | 9.3 | 5.58 | | |
| 41 | original | 64 | 22 | 43.0 | 21.0 | 25.0 | | 0.52 | 19.2 | 9.98 | | 8.8 | 6.59 | 29.6 | #5.5 |
| | new hammer, shank & whippen, cut punching | 60 | 29 | 44.5 | 15.5 | 15.6 | | 0.52 | 16.6 | 8.63 | | 9.2 | 5.59 | | #6.5 |
| | rebalance | 56 | 25 | 40.5 | 15.5 | 19.6 | | 0.52 | 16.6 | 8.63 | | 9.2 | 5.59 | | |

Original, Actual test and proposed rebalance



Calculate Mol of the keys

❖ 目標

| | 3 | B0 | measured of | original FW | | 29.8 | | | | | | | | | | | |
|-------------|------------------|-------|--------------------|---------------------------|----------------------|------------------------|--------------------------|-------------------------|--------------------|-------------------------|--------------------|-------------------------|--------------------|-------------------------|--------------------|-------------------------|-------------------|
| a | 3 | B0 | calculated of | original FW | | 34.9 | front | 55.1 | back | 20.2 | differe | nce | -5.1 | | | | |
| b | | | least inertia wi | ith new FW | | 32.7 | front | 53.0 | back | 20.2 | aiming | FW | 32.7 | | | | |
| С | | econo | mical setting wi | ith new FW | | 32.7 | front | 52.9 | back | 20.2 | aiming | FW | 32.7 | | | | |
| d | | | | | | 32.7 | front | 52.9 | back | 20.2 | aiming | FW | 32.7 | | | | |
| | | | | | | | | | | | | | | | | | |
| | Yuji | 's M | oment of i | nertia f | or ke | y cal | culatir | ng ch | art | | Los | d /fra | n+\ | | | | |
| | Yuji | 's M | oment of i | nertia f | or ke | y cal | culatir | ng ch | art | | Lea | d (fro | ont) | | | | |
| | Yuji Key # | Note | oment of i | Whole Inertia | FW point distn | Center of torque | COG position | distan ce #5 (mm) | mass of lead | distan ce #4 (mm) | | distan ce #3 (mm) | mass of lead | distan ce #2 (mm) | mass of lead | distan ce #1 (mm) | mas of lead |
| a | Key | | 200 | Whole | FW point | Center of | COG | distan ce #5 | mass of | ce #4 | mass of | distan ce #3 | mass of | ce #2 | of | ce #1 | of |
| _ | Key # | Note | Status | Whole Inertia | FW point distn | Center of torque | COG position | distan ce #5 (mm) | mass of lead | ce #4 (mm) | mass of lead | distan ce #3 (mm) | mass of lead | ce #2 | of | ce #1 | of lea |
| a b c | Key # | Note | Status Original | Whole Inertia 38816 | FW point distn | Center of torque | COG position 0.676 | distan ce #5 (mm) | mass of lead | ce #4 (mm) 176 | mass of lead | distan ce #3 (mm) | mass of lead | ce #2 (mm) | of lead | ce #1 (mm) | of |

Positioning of the key leads

- Needs more key leads when locating near to balance pin
- More MoI when locates key leads to farer than pin
- Watch CoG to even MoI

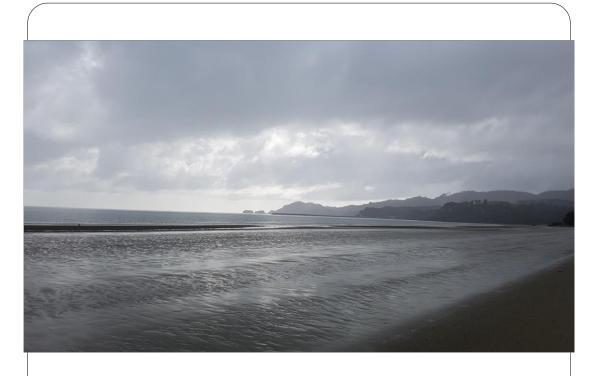
| | | | | | | | | Lea | ad (fro | nt) | | | | |
|---------------|------------------|----------------------|------------------------|-----------------|-------------------------|--------------------|-------------------------|--------------------|-------------------------|--------------------|-------------------------|--------------------|-------------------------|--------------------|
| Status | Whole Inertia | FW point distn | Center of torque | COG position | distan ce #5 (mm) | mass of lead | distan ce #4 (mm) | mass of lead | distan ce #3 (mm) | mass of lead | distan ce #2 (mm) | mass of lead | distan ce #1 (mm) | mass of lead |
| Original | 38816 | 247 | 175.7 | 0.676 | 198 | 11.2 | 176 | 11.2 | 153 | 11.2 | | | | |
| least inertia | 33417 | 247 | 85.2 | 0.328 | | | 135 | 6.0 | 110 | 19 | 80 | 19 | 50 | 19.0 |
| economical | 36057 | 247 | 135.8 | 0.522 | | ř | 176 | 11.2 | 153 | 11.2 | 98 | 17 | | |

7% reduction

Check how Mol is set

| | How r | noment | of inert | ia char | nges | | |
|-----------------------------------|------------|--------------|----------------|--------------|----------------|--------|--------------|
| | | Hammer | H at key | Whip | W at key | Key | Whole action |
| Expecting Moi after modification | | 1,825 | 152,190 | 756 | 3,263 | 36,057 | 191,511 |
| % deducted from original | | 4% | | 0% | | 7% | 8% |
| Existing Moi (gcm^2) | | 1,893 | 164,973 | 756 | 3,411 | 38,816 | 207,199 |
| HSW (g) | original | 11.2 | g | | | | 1 |
| | new | 10.8 | g | | | | |
| Hammer distance (cm) | original | 13 | cm | | | | |
| distance between balance hole co | enter and | center at th | e top of cap | stan screv | V | | |
| | 13.7 | cm | 13.4 | cm | | | |
| distance between center at the to | p of capst | an screw a | nd whippen | center | | | |
| | 6.45 | cm | 6.15 | | | | |
| distance between whippen center | and 1mm | forward fro | om back side | e of the jac | ck at top of j | ack | |
| | 9.45 | cm | | | | | / |
| distance between shank flange co | enter and | connecting | point at rolle | er leather v | vith jack | | / |
| | 2.15 | cm | | | | | |

8% of MoI reduction is expectable



Golden Bay, South island, New Zealand